

APPENDIX III

CLAIM No.	Serial No. 08/840,893
<p>73. A coated optical fiber comprising:</p> <p>an optical fiber; and</p> <p>a cured primary coating on the optical fiber</p> <p>wherein the primary coating is strippable from a portion of the optical fiber</p> <p>at a temperature in at least a portion of the temperature range from about 25° to about 125° C</p> <p>by exerting a force to a portion of the primary coating about the portion of optical fiber in a direction parallel to the longitudinal axis of the glass fiber which is away from a portion of the primary coating remaining on the optical fiber, such that the exertion of force,</p> <p>followed by an optional one wipe with an alcohol laden piece of cloth or paper of the stripped portion of the optical fiber,</p> <p>results in a stripped portion of optical</p>	<p>Original claim 91 (page 138, lines 20-21) is directed to "A coated optical ... fiber." Page 1, lines 10-11 ("The invention also relates to coated optical glass fibers ...")</p> <p>A cured primary coating is disclosed at page 32, lines 1-2 ("compositions were suitably cured by exposure to UV light ..."); page 47, lines 14-16 ("cured by exposure to UV light to form cured coatings.")</p> <p>Original claims 209, 210, are representative of claims describes a primary coating that is strippable from a portion of the optical fiber, where strippability is described in terms of fiber pull-out friction and predicted strip cleanliness.</p> <p>Strippability of the primary coating is described on page 8, lines 1-6 ("... to allow the inner primary coating to slide readily off from the optical glass fiber ... when a stripping force ... is applied ...")</p> <p>The temperature is described on page 32, lines 2-3 ("The dL/L for each coating was measured over the temperature range of 25 C (ambient temperature) to 125 C (highest usual stripping temperature).")</p> <p>A stripping method is disclosed on page 2, line 35 to page 3, line 15 and page 16, line 32 to page 17, line 7 ("When a typical ribbon stripping tool is applied to a ribbon assembly, pressure is applied to the ribbon assembly between heated plates. At the ends of the plates near the cut made in the matrix material and the inner and outer primary coatings, the inner primary coating can form an initial delamination site on the optical glass fiber, shown at 27 and 28 [in Fig. 1].")</p> <p>An optional one wipe with alcohol is disclosed in the article by Mills (the "Mills test") which is incorporated by reference at page 6, lines 23-28.</p> <p>The results of stripping is disclosed on page 8,</p>

CLAIM No.	Serial No. 08/840,893
<p>fiber having substantially no residue of the primary coating.</p>	<p>lines 2-4 (“...while leaving substantially no residue on the surface of said optical glass fiber during ribbon stripping”); page 48, lines 2-4 (“Microscopic examination of the pulled-out fibers at low magnification (e.g., 10X) clearly revealed the presence or absence of debris on the glass surface. If debris was present, the amount of debris was noted”).</p>
<p>74. The coated optical fiber of claim 73, wherein the primary coating is strippable at the temperature upon execution of the force,</p> <p>to leave a stripped portion of the optical fiber having a Mill’s value of about 2 or less.</p>	<p>See, claim 1 (page 121, lines 15-25) (“a fiber friction force level ... to permit the inner primary coating to slide off the optical glass fiber ... when a stripping force is ... applied ...”); and claim 2 (page 121, lines 28-30 (“...wherein said stripping force is ... at a ribbon stripping temperature.”)).</p> <p>The Mills’ test values represent strip cleanliness, (page 55, lines 14-20: “When referring to strip cleanliness and predicted strip cleanliness herein, the numerical values correspond to those of the Mill’s test.”). Values of about 2 or less are described on page 100, lines 2-3.</p>
<p>75. The coated optical fiber of claim 73, wherein the primary coating is strippable at the temperature upon exertion of the force to leave</p> <p>a stripped portion of the optical fiber having a Mill’s test value of 1.5.</p>	<p>See, claim 1 (page 121, lines 15-25) (“a fiber friction force level ... to permit the inner primary coating to slide off the optical glass fiber ... when a stripping force is ... applied ...”); and claim 2 (page 121, lines 28-30 (“...wherein said stripping force is ... at a ribbon stripping temperature.”)).</p> <p>A Mills’ test value of 1.5 is described on page 56, Table 5, Coating F, Rating (Mill’s Value 1.5) and page 77, Table 8 (Ex. 4-5, 4-7, 4-11, 4-12 all values were 1.5).</p>
<p>76. The coated optical fiber of claim 73,</p>	<p>The coatings prior to curing are liquid at 60</p>

CLAIM No.	Serial No. 08/840,893
wherein the coating prior to curing is liquid at 60° C.	°C, as shown by the measurement of viscosity at 25 °C, as shown on page 68, Table 6, (viscosity of primary coating compositions at 25 °C, in the range of 6760 to 7650 mPa.s; similar viscosity values at 25 °C for the primary coating compositions in Tables 7, 8, 9 and 10).
77. The coated optical fiber of claim 76, wherein the coating prior to curing is liquid at 25 °C.	The coatings prior to curing are liquid at 25 °C, as shown by the measurement of viscosity at 25 °C: page 68, Table 6, (viscosity of primary coating compositions at 25 °C, in the range of 6760 to 7650 mPa.s; similar viscosity values at 25 °C for the primary coating compositions in Tables 7, 8, 9 and 10).
<p>78. The coated optical fiber of claim 73,</p> <p>wherein the primary coating is made of a material which is removable from a glass substrate by an adhesion test force of less than 45 g/in, as measured by a peel back test at 50% relative humidity,</p> <p>has an elongation to break of at least about 88% as measure by ASTM D-638, and</p> <p>has a tensile strength of at least about 72.5 psi as measured by ASTM D-638.</p>	<p>The adhesion force (at 50% RH) of 45 g/in is shown in Ex. 2-2, Table 3, page 50; and an adhesion test force of less than 45 g/in. is shown in Ex. 2-3, Table 3, page 50.</p> <p>An elongation to break of at least about 88% is shown by the examples: Table 8, page 76, Elongation: 100% to 180% (Ex. 4-8, 4-9 and 4-10); Table 9, page 82, Elongation: 88% (Ex. 5-2).</p> <p>A tensile strength of 72.5 psi is disclosed in Ex. 5-2, Table 9, page 82 (0.5 MPa = 72.5 psi); Tensile strengths greater than 72.5 are disclosed for the primary coatings from Table 8, page 76: Ex. 4-8 (1.5 MPa = 218 psi); Ex. 4-9 (0.6 MPa = 87 MPa); Ex. 4-10 (1.1 MPa = 160 psi).</p>
79. The coated optical fiber of claim 78, wherein the adhesion test force is about 14 g/in.	An adhesion test force of 14 g/in is disclosed in Table 3, page 50, for Ex. 2-3: Adhesion at 50% RH = 14 g/in.
80. The coated optical fiber of claim 73, wherein the primary coating is made of a	

CLAIM No.	Serial No. 08/840,893
<p>material which is removable from a glass substrate by an adhesion force of at least 5 g/in, as measured by a peel back test at 95% relative humidity,</p> <p>has an elongation to break is a least about 88% as measured by ASTM D-638, and</p> <p>has a tensile strength of at least about 72.5 psi as measured by ASTM D-638.</p>	<p>95% RH adhesion values are disclosed in Table 3, page 52, adhesion force = 12 or 34 g/in at 95% RH (Ex. 2-3 and Ex. 2-2).</p> <p>Elongation at break (measured by ASTM D-638M) of 88% is disclosed in Table 9, page 82, Ex. 5-2: Elongation = 88%; higher values are disclosed for examples Ex. 4-8 to 4-10 in Table 8, page 76.</p> <p>A tensile strength of at least about 72.5 psi is shown in Table 9, page 82, Ex. 5-2: (Tensile Strength = 0.5 MPa = 72.5 psi). Higher tensile strength values are shown in other examples: Ex. 5-4 (Tensile Strength = 1.1 MPa = 159.5 psi); Ex. 4-8 (Tensile Strength = 1.5 MPa = 217.5 psi) (Table 8, page 76).</p>
<p>81. The coated optical fiber of claim 78, wherein the elongation to break is about 140%.</p>	<p>The elongation to break of 140% is disclosed in Table 8 (cont), page 76; Ex. 4-9.</p>
<p>82. The coated optical fiber of claim 78, wherein the tensile strength is at least about 145 psi.</p>	<p>A tensile strength of 145 psi is disclosed in Example 4-1 in Table 7, page 73 (1 MPa = 145 psi). Higher tensile strength values are disclosed in Examples 4-8 (1.5 MPa = 217.5 psi) and 4-10 (1.1 MPa = 159.5 psi).</p>
<p>83. The coated optical fiber of claim 73,</p> <p>wherein said primary coating layer comprises</p> <p>a cured reaction product of from about 5 to about 80 percent by weight of one or more acrylate- or methacrylate- terminated urethane oligomers.</p>	<p>A primary coating layer which is the cured reaction product of from about 5 to about 80 wt.% of oligomers is disclosed on page 94, lines 24-26.</p> <p>Acrylate- or methacrylate terminated urethane oligomers are disclosed on page 93, line 30 to page 94, line 9 ("...oligomers according to the invention can be made, for example, by reacting ... a diisocyanate compound ... with a long chain alkyl containing a hydroxy functional group and a radiation-curable functional group The urethane linking group ... is formed by the reaction of the isocyanate group with a hydroxyl group. In a second reaction the remaining isocyanate group is reacted with the as yet unreacted</p>

CLAIM No.	Serial No. 08/840,893
	hydroxyl group of the compound. ... Suitable examples of reactants containing a radiation-curable functional group and a hydroxy group are hydroxyethyl-acrylate or 2-hydroxypropylacrylate.").
<p>84. The coated optical fiber of claim 83, wherein said primary coating layer comprises a cured reaction product of,</p> <p>in addition to the acrylate or methacrylate-terminated oligomer</p> <p>from about 0.1 to about 20 percent by weight of</p> <p>a monomer selected from the group consisting of isobornyl acrylate,</p> <p>isodecyl acrylate,</p> <p>hexanediol diacrylate,</p> <p>phenoxyethyl acrylate, and</p> <p>lauryl acrylate.</p>	<p>Disclosure of a primary coating layer comprising a cured reaction product of from about 0.1 to about 20% by weight of additional monofunctional monomers is found on in Ex. 6-1 (5%) (page 87, Table 10), Ex. 10-12 (20.1%) (page 106, Table 15).</p> <p>Isobornyl acrylate is disclosed on page 104, line 31.</p> <p>Isodecyl acrylate is disclosed on page 82, Table 9 (Ex. 5-1, Ex. 5-3).</p> <p>Hexanediol diacrylate is disclosed on page 103, line 30.</p> <p>Phenoxyethyl acrylate is disclosed on page 89, Table 11, Ex. 10-22.</p> <p>Lauryl acrylate is disclosed on page 104, line 32.</p>
<p>85. The coated optical fiber of claim 83 wherein</p> <p>said primary coating layer additionally comprises about 1.0 wt% of an organofunctional silane adhesion promoter.</p>	<p>The disclosure of organofunctional silane adhesion promoter is found on page 35, line 29 through page 38, line 27: ("... 'glass coupling moiety' ... is understood to mean a functional group which ... has the ability to improve adhesion to an inorganic surface or at an inorganic surface", "Silane coupling moieties are preferred."</p> <p>An amount of 1.0 wt.% is disclosed on page 68, Table 6, gamma-mercaptopropyl trimethoxy silane (1 part by weight of 100 parts).</p>
86. The coated optical fiber of claim 85,	The mercapto-functional silanes are disclosed

CLAIM No.	Serial No. 08/840,893
wherein said adhesion promoter is a mercapto-functional silanes.	on page 37, lines 29-31 ("Common organic functionalities of the silane agents include, for example, ... mercapto, ...").
87. The coated optical fiber of claim 85, wherein said adhesion promoter is 3-mercaptopropyltrimethoxy-silane.	3-mercaptopropyltrimethoxysilane is disclosed on page 68, Table 6 (Ex. 3-1 to 3-4).
88. The coated optical fiber of claim 83, wherein said primary coating layer additionally comprises a photoinitiator.	The addition of a photoinitiator is disclosed on page 45, line 6 ("at least one photoinitiator").
89. The coated optical fiber of claim 83, wherein said primary coating layer additionally comprises from about 0.5 percent by weight of thiodiethylene bis(3,5-di-tert-butyl-4-hydroxy cinnamate .	A disclosure of about 0.5 percent by weight of thiodiethylene bis(3,5-di-tert-butyl-4-hydroxy cinnamate is in Ex. 2-4 on page 52, Table 4 (0.5%).
<p>90. The coated optical fiber of claim 73, wherein</p> <p>the primary coating comprises the radiation-cured reaction product of the following ingredients:</p> <p>(A) from about 5 percent to about 80 percent by weight of</p> <p>a reactively terminated urethane oligomer which is</p> <p>the reaction product of</p> <p>(i) polyether polyol;</p> <p>(ii) a wholly aliphatic polyisocyanate;</p> <p>and</p> <p>(iii) an endcapping monomer supplying a reactive terminus;</p>	<p>A disclosure of "...a radiation-curable inner primary coating composition containing at least one radiation-curable urethane oligomer comprising at least one polymeric block and at least one functional group capable of polymerization in the presence of actinic radiation connected to said at least one polymeric block" is found on page 11, lines 17-22.</p> <p>The amount of linear oligomer can be from about 5 to about 80 wt.% (page 91, lines 22-23).</p> <p>A disclosure of reactively terminated urethane oligomers is found on page 41, line 32- page 42, line 2: "Representative linking compounds include diisocyanate compounds, wherein linkage occurs by formation of urethane, ... by reaction of hydroxyl, ... with isocyanate ... although aliphatic diisocyanates are preferred."</p> <p>Endcapping monomers supplying a reactive terminus are shown by the formula on page 90, lines 25 et seq., as linear oligomers to</p>

CLAIM No.	Serial No. 08/840,893
<p>(B) from about 15 percent to about 65 percent by weight of ethoxylated nonyl phenol acrylate;</p> <p>(C) from about 1.5 percent to about 3 percent by weight of a photoinitiator; and</p> <p>(D) about 1 percent by weight of an organofunctional silane adhesion promoter which binds in with the primary coating composition during cure;</p>	<p>improve ribbon stripping operations:</p> <p>$R^1 - L - [R^2 - L]_n - R^3$, where R^1 and R^3 are organic groupings having radiation curable functional groups; R^2 is an organic radical, L is a linking group, and $[R^2 - L]_n$ can contain polyether.</p> <p>See also page 92, lines 10 et seq. for the radiation-curable oligomer of formula $R^4 - x - L - x - [R^5 - x - L - x]_n - R^6$, where R^4 is a substantially linear long chain alkyl terminating in at least one hydroxyl group; L represent a molecular bridging group preferably derived from a diisocyanate precursor, x represent resulting reacting linking group, e.g., urethane, R^5 is a linear or branched or cyclic hydrocarbon or polyether moiety derived from a diol, and can contain a branched or cyclic aliphatic group, R^6 is an end group carrying a radiation-curable functional group.</p> <p>See also, e.g., page 101, lines 10-12 ("The radiation-curable oligomer can be easily formed by reacting a polymeric polyol, a compound containing a radiation-curable functional group and a hydroxyl group, and a polyisocyanate."); page 101, lines 18-21 (examples of polymeric polyols include polyether diols); page 102, lines 33-36, et seq. for organic polyisocyanates, including the wholly aliphatic polyisocyanates and examples in Table 15 to Table 21 on pages 106-118.</p> <p>A disclosure of the inner primary coating composition including (B) ethoxylated nonylphenol acrylate between about 15% and about 65% is found in Ex. 10-22, Table 11, page 89 (15.1%) and Ex. 3-1, Table 6, page 68 (64.4%).</p> <p>From about 1.5 to about 3% of photoinitiator (C) photoinitiator is found in Table 8, page 75, Ex. 4-11 (1%), Ex. 4-9 (3%).</p> <p>About 1% of (D) organofunctional silane adhesion promoter is disclosed in Examples 3-1 to 3-4 in Table 6, page 68.</p> <p>The disclosure of the sums of the amounts</p>

CLAIM No.	Serial No. 08/840,893
<p>wherein all of the stated percentages are percentages by weight based on the total weight of the primary coating prior to cure,</p> <p>wherein the tensile modulus of the coating composition, when cured, is less than about 220 psi at 25° C, and</p> <p>wherein the refractive index of the cured coating composition is suitable for an optical fiber coating.</p>	<p>based on the total weight of the primary coating prior to cure is seen from the data in the Tables wherein the total of the ingredients was 100 wt.%.</p> <p>A disclosure of tensile modulus values of less than about 220 psi at 25°C is found in Table 8, page 76: Ex. 4-5 (1.2 MPa = 174 psi); Ex. 4-9 (1.1 MPa = 160 psi) and Ex. 4-10 (1.3 MPa = 188.5 psi).</p> <p>A disclosure of refractive index suitable for an optical coating is inherent throughout the specification. Formation of "clear" films suitable for an optical fiber coating are disclosed in Table 6, page 68.</p>
<p>91. The coated optical fiber of claim 73,</p> <p>wherein the primary coating comprising the radiation-cured reaction product of the following ingredients:</p> <ul style="list-style-type: none"> (1) from about 5 to about 80 percent by weight of an acrylate-terminated aliphatic polyether urethane oligomers; (2) from about 15 to about 65 percent by weight of ethoxylated nonyl phenol acrylate; (7) from about 1.5 to about 3 percent by weight of a photoinitiator; and (8) about 1 percent by weight of an organofunctional silane adhesion promoter which binds in with the primary coating composition during cure; <p>wherein all of said percentages being percentages by weight based on the weight of the primary coating prior to cure.</p>	<p>See discussion for Claim 90 for the support for claim 91.</p>
<p>92. The coated optical fiber of claim 91,</p> <p>wherein said primary coating is obtained by</p>	<p>The coatings prior to curing are liquid at 25 °C, as shown by the measurement of viscosity at 25 °C: page 68, Table 6, (viscosity of primary coating compositions at 25 °C, in the</p>

CLAIM No.	Serial No. 08/840,893
curing a composition that is liquid at 25° C.	range of 6760 to 7650 mPa.s; similar viscosity values at 25 °C for the primary coating compositions in Tables 7, 8, 9 and 10).
<p>93. An optical ribbon comprising</p> <p>a plurality of optical fibers of claim 73 and a matrix material, the plurality of fibers held together in a parallel arrangement by the matrix material.</p>	<p>A ribbon assembly comprising a plurality of coated optical fibers, at least one optical glass fiber coated with at least an inner primary coating and a matrix material bonding the plurality of coated optical fibers together is the subject matter of original claim 1.</p> <p>A disclosure of ribbon assemblies is found on page 1, lines 11-13 and page 119, lines 10 et seq.</p>
<p>94. A method of preparing a coated optical fiber for splicing,</p> <p>the coated optical fiber being a coated optical fiber according to claim 73,</p> <p>comprising the steps of:</p> <p>stripping the primary coating away from a portion of the optical fiber at a temperature in at least a portion of the temperature range from about 25° to about 125° C. by cutting with a blade into the primary coating,</p> <p>then having the blade exert a force on the primary coating in a direction parallel to the optical fiber to force the primary coating away from the portion of the optical fiber,</p> <p>and optionally wiping the portion of optical fiber from which primary coating has been forced away with an alcohol laden piece of cloth or paper,</p> <p>such that the stripped portion exhibits little or no residue of the primary coating.</p>	<p>A disclosure of a method for preparing a coated optical fiber for splicing including ribbon stripping is found on page 2, lines 35 et seq.</p> <p>The temperature of 25 to 125 °C is found on page 32, lines 1-4.</p> <p>A disclosure of the optional wiping step is found in the Mills' test incorporated by reference into the application on page 7, lines 6-11.</p> <p>The result of stripping is disclosed on page 8, lines 2-4 ("...while leaving substantially no residue on the surface of said optical glass fiber during ribbon stripping"); page 48, lines 2-4 ("Microscopic examination of the pulled-out fibers at low magnification (e.g., 10X) clearly revealed the presence or absence of debris on the glass surface. If debris was</p>

CLAIM No.	Serial No. 08/840,893
<p>95. A method of splicing coated optical fibers comprising, preparing two optical fibers for splicing according to the method of claim 94;</p> <p>aligning the stripped portions of the prepared optical fibers; and</p> <p>joining the stripped portions of the prepared optical fibers.</p>	<p>present, the amount of debris was noted”).</p> <p>A method for connecting optical fibers individually or as ribbon assemblies for “mass fusion splicing operation” is disclosed on page 2, lines 17-28.</p>
<p>96. A spliced optic fiber made by the method of claim 95.</p>	<p>A disclosure of a spliced optic fiber by the splicing operation is found on page 2, lines 23-34.</p>
<p>97. A coated optical fiber comprising:</p> <p>an optical fiber;</p> <p>a primary coating coated onto the optical fiber, the primary coating made of a material which is removable from a glass substrate by an adhesion test force of less than 45 g/in, as measured by a peel back test at 50% relative humidity</p> <p>an elongation of at least about 88% as measured by ASTM D-638, and</p> <p>a tensile strength of at least about 72.5 psi as measured by ASTM D-638.</p>	<p>A coated optical fiber comprising an optical fiber and primary coating is disclosed on page 8, lines 20-22.</p> <p>Examples 2-2 and 2-3 (Table 3, page 50) show that the invention encompasses coatings having an adhesion force at 50% RH of 45 g/in or less is disclosed in Table 3, page 50.</p> <p>An 88% elongation is disclosed in Example 5-3 on page 82 in Table 9; ASTM D-638M is disclosed on page 58, line 1 to page 60, line 21.</p> <p>A tensile strength of 72.5 psi, is disclosed as 0.5 MPa in Example 5-2 on page 82 in Table 9. The conversion from MPa to psi (1 MPa = 145 psi) can be found on page 59, line 7.</p>
<p>98. A process for preparing a coating optical fiber comprising</p> <p>(1) applying to an optical fiber a primary coating composition layer comprising a mixture of the following ingredients:</p> <p>(A) from about 5 percent to about 80 percent by weight of a reactively terminated urethane oligomer which is the reaction product of (i) a polyether polyol; (ii) a wholly aliphatic polyisocyanate; and (iii) an endcapping monomer supplying a reactive terminus;</p>	<p>A process for preparing a coated optical fiber by applying a primary coating composition to the optical fiber is shown generally throughout the specification and examples, including, page 1, lines 28-30; page 46, lines 4-6 (including the disclosure of incorporated patents 4,474,830 and 4,913,859).</p> <p>Compositions with ingredients (A), (B), (C) and (D) are also described throughout the specification. A reactively terminated urethane oligomer (see, e.g., the formulas on page 42, lines 20 et seq.; page 90, lines 25 et seq.; page 92, lines 10 et seq.) wherein the linking group L or x is preferably urethane</p>

CLAIM No.	Serial No. 08/840,893
<p>(B) from about 15 percent to about 65 percent by weight of ethoxylated nonyl phenol acrylate;</p> <p>(C) from about 1.5 percent to about 3 percent by weight of a photoinitiator; and</p> <p>(D) about 1 percent by weight of an organofunctional silane adhesion promoter which binds in with the primary coating composition during cure;</p> <p>wherein all of the stated percentages are percentage by weight based on the total weight of the primary coating prior to cure,</p> <p>wherein the tensile modulus of the coating composition when cured, is less than about 220 psi at 25° C., and</p>	<p>(e.g., page 42, lines 35; page 90, line 32; page 93, line 5).</p> <p>The reaction of a mixture of (i) polyether polyol, (ii) wholly aliphatic diisocyanate and (iii) end-capping monomer supplying a reactive terminus, is shown in Examples (e.g., page 50, Table 3, Oligomer C: reaction product of (i) polytetramethylene ether glycol, (ii) isophorone diisocyanate, and (iii) hydroxyethylacrylate and mercaptosilane) and is also generally disclosed on page 101, lines 10-13 ("The radiation-curable oligomer can be easily formed by reacting a polymeric polyol, a compound containing a radiation-curable functional group and a hydroxyl group, and a polyisocyanate."); page 101, lines 18-19 (examples of polymeric polyols include polyether diols); page 102, lines 34-36, et seq. for organic polyisocyanates, including the wholly aliphatic polyisocyanates and examples in Tables 15-21 on pages 106 to 118. The range of about 5 to about 80% is disclosed on page 94, line 25.</p> <p>The Examples on page 50, Table 3, also include (B) ethoxylated nonyl phenol acrylate; (C) photoinitiator; and (D) organofunctional silane, at or within the stated ranges.</p> <p>The range of about 15% to 65% for reactant (B) is found in the examples, e.g., page 89, Table 11; page 68, Table 6, respectively. The range of about 1.5% to about 3% for reactant (C) is found in the examples, e.g., page 31, Table 1 (1.54%); page 89, Table 11 (3%).</p> <p>The amount of 1% of the organosilane adhesion promoter is 1% in the composition of Example 10-22, page 89, Table 11.</p> <p>All amounts are based on 100 wt%.</p> <p>The tensile modulus of the cured composition of less than about 220 psi is shown to be part of the invention by reference to, for example,</p>

CLAIM No.	Serial No. 08/840,893
<p>wherein the refractive index of the cured coating composition is suitable for an optical fiber coating;</p> <p>and</p> <p>(2) radiation-curing said coating in situ,</p> <p>wherein the primary coating is strippable from a portion of the optical fiber at a temperature in at least a portion of the temperature range from about 25° to about 125° C. by exerting a force to a portion of the primary coating in a direction parallel to the longitudinal axis of the glass fiber which is away from a portion of the primary coating remaining on the optical fiber, such that the exertion of force followed by an optional one wipe, with an alcohol laded piece of cloth or paper of the stripped portion of optical fiber, results in the stripped portion of optical fiber having a substantially no residue of the primary coating.</p>	<p>Example 4-1, on page 73, Table 7 (1.4 MPa = 203 psi); Ex. 4-5, Ex. 4-9 and Ex. 4-10, on page 76, Table 8 (CONT) with values of 174 psi (1.2 MPa), 160 psi (1.1 MPa) and 188.5 psi (1.3 MPa), respectively.</p> <p>The refractive index being suitable for an optical coating, is implicit throughout the disclosure and is exemplified by the clear films obtained in Examples 3-1 to 3-4, on page 68, Table 6.</p> <p>The step of radiation-curing in situ is also implicit throughout the disclosure and is shown, for example, on page 34, lines 1-2 and page 49, lines 34-36.</p> <p>That the primary coating is strippable at the temperature ranges and under the conditions specified, with substantially no residue of the primary coating is disclosed throughout the specification, for example, page 32, lines 2-4 for the temperature range of 25° to 125° C; and Ex. 2-1, on page 48, Table 2, for "no residue." The optional one wipe with alcohol is disclosed in the incorporated Mills test disclosure as stated on page 6, lines 23-28.</p>